

Hierarchal Models for the analysis of a power buss

In some cases where the simulation circuit would get to big or cluttered with details it is wise to use a hierarchal approach in a simulation. The hierarchal approach allows the user to bury details into subcircuits and build commonly used elements once. However, there may still a desire to have some control over the subcircuit at the top level of the simulation circuit.

This presentation will demonstrate the hierarchal approach by way of a using a twisted pair RLGC model whose electrical characteristics can be modified with a single dimensional parameter (length). Also, the approach to translate a SPICE deck into an AWB simulation will be shown for a new hierarchal subcircuit model.



Hierarchal Models for the analysis of a power buss

We would like to simulate the power buss of a system and include detailed models of the wires and subsystems. To do this it makes sense to build hierarchal models for each wire and subsystem and then interconnect them in a hierarchal simulation.

The wire model will use the RLGC lossy lumped element twisted pair model with a slight modification for grounding and will change electrical characteristics as a function of wire length.

One subsystem model which has been supplied to us as an Intusoft SPICE model will be translated into the proper AWB format and integrated into the hierarchal simulation



Hierarchal Models for the analysis of a power buss

We have reviewed the literature and found a model for a twisted pair.

TRANSMISSION LINE MADE FROM TWISTED PAIR WIRE

Formulas included in this spreadsheet:

- Twisted-pair characteristic impedance
- Twisted-pair propagation delay
- Twisted-pair inductance
- Twisted-pair capacitance

Variables used:

- d Diameter of wire (in.)
- s Separation between wires (in.)
- x Length of wire (in.)
- er Effective relative dielectric constant of medium between wires
- AWG American wire gauge
- temp Temperature (°C)
- ρ Bulk resistivity of copper
- δρ Thermal coefficient of resistance
- ρ := 6.787 · 10⁻⁷ ohm-in.
- δρ := .0039 per deg. C
- temp := 20
- awg := 16
- x := 12
- s := .068
- er := 2.55

In our case the temperature coefficient of the wire will be ignored, i.e. temp will be set equal to 20°C.

This MathCAD program is used to calculate the R, L and C values for the wire we would like to model.

Conversions between American Wire Gauge (AWG) and diameter (in.):

$$DIAMETER(awg) := 10^{-\frac{awg+10}{20}}$$

$$DIAMETER(16) = 0.0501$$

$$d := DIAMETER(16)$$

$$AWG(d) := -10 - 20 \cdot \log(d)$$

General formula for resistance of a round wire (Ω):

$$RROUND(d,x,temp) := \frac{4 \cdot \rho \cdot x}{\pi \cdot d^2} [1 + (temp - 20) \cdot \delta\rho]$$

Resistance of a round wire specified by AWG size instead of diameter (Ω):

$$RROUND_AWG(awg,x,temp) := RROUND(DIAMETER(awg),x,temp)$$

Characteristic impedance of twisted pair (Ω):

$$ZTWIST(d,s,er) := \frac{120}{\sqrt{er}} \cdot \ln\left(\frac{2 \cdot s}{d}\right)$$

Propagation delay per in. twisted pair (s/in.):

$$PTWIST(er) := 84.72 \cdot 10^{-12} \cdot \sqrt{er}$$

Inductance of twisted pair (H):

$$LTWIST(d,s,x) := x \cdot 10.16 \cdot 10^{-9} \cdot \ln\left(\frac{2 \cdot s}{d}\right)$$

Capacitance of twisted pair (F):

$$CTWIST(d,s,er,x) := \left(\frac{x \cdot 7065 \cdot 10^{-12}}{\ln\left(\frac{2 \cdot s}{d}\right)}\right) \cdot er$$

Using this program the user could determine new R, L and C values based upon other wire types. Or the model could also be changes to pass these wire parameters.

Resistance of a round wire specified by AWG size instead of diameter (Ω):

$$RROUND_AWG(awg,x,temp) = 4.1283 \times 10^{-3}$$

Characteristic impedance (Ω):

$$ZTWIST(d,s,er) = 75.0162$$

Total inductance (H):

$$LTWIST(d,s,x) = 1.2171 \times 10^{-7}$$

Same result in nH:

$$LTWIST(d,s,x) \cdot 10^9 = 121.7079$$

Inductance per in. (H):

$$LTWIST(d,s,1) = 1.0142 \times 10^{-8}$$

Total capacitance (F):

$$CTWIST(d,s,er,x) = 2.1657 \times 10^{-11}$$

Same result in pF:

$$CTWIST(d,s,er,x) \cdot 10^{12} = 21.6566$$

Capacitance per in. (F):

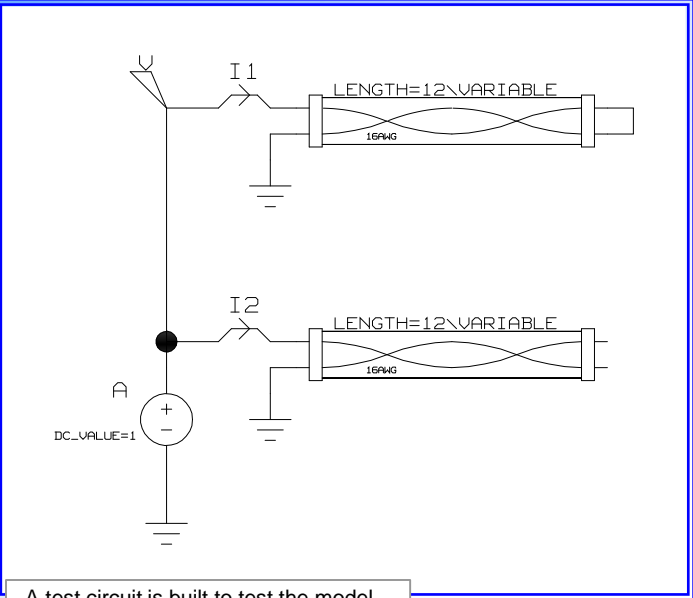
$$CTWIST(d,s,er,1) = 1.8047 \times 10^{-12}$$

Build our model and compare our electrical characteristic to the calculated values.



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A subcircuit model is built and shows that for a 1 foot length of wire the simulation results match the expected results.



A test circuit is built to test the model. In this case the R, L and C will be measured as well as the characteristic impedance Z_0

Resistance of a round wire specified by AWG size instead of diameter (Ω):

$$RROUND_AWG(awg,x,temp) = 4.1283 \times 10^{-3}$$

equals 2X for two wires

Characteristic impedance (Ω):

$$ZTWIST(d,s,er) = 75.0162$$

Total inductance (H):

$$LTWIST(d,s,x) = 1.2171 \times 10^{-7}$$

Same result in nH:

$$LTWIST(d,s,x) \cdot 10^9 = 121.7079$$

Inductance per in. (H):

$$LTWIST(d,s,1) = 1.0142 \times 10^{-8}$$

Total capacitance (F):

$$CTWIST(d,s,er,x) = 2.1657 \times 10^{-11}$$

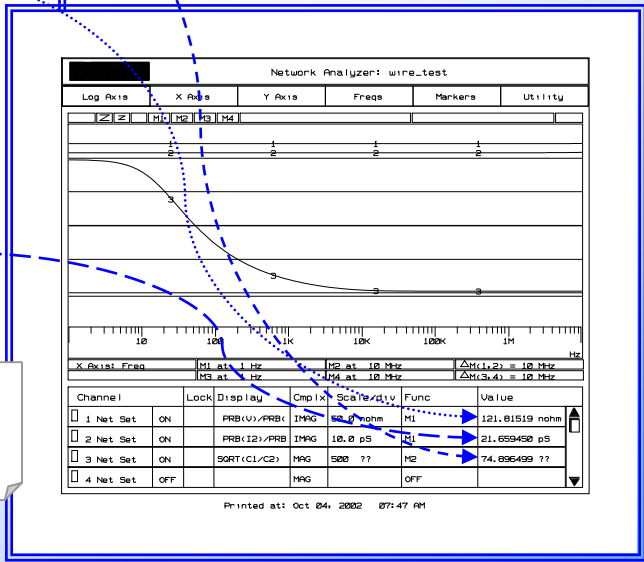
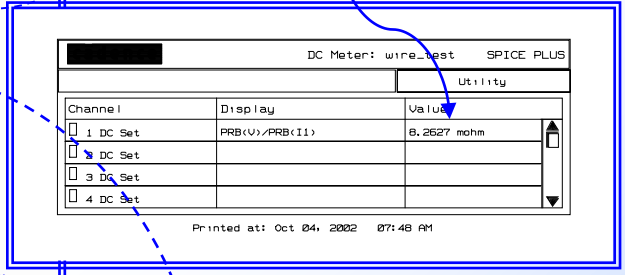
Same result in pF:

$$CTWIST(d,s,er,x) \cdot 10^{12} = 21.6566$$

Capacitance per in. (F):

$$CTWIST(d,s,er,1) = 1.8047 \times 10^{-12}$$

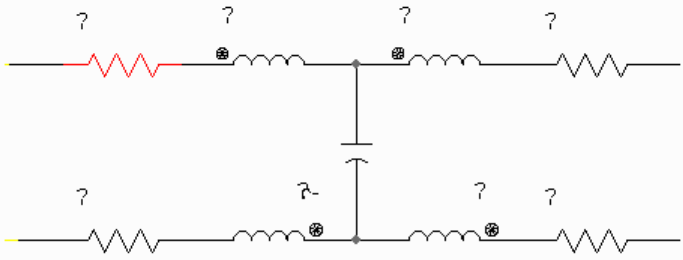
As can be seen there is a good match between the MathCAD program and AWB simulation results. The model is validated and can be used for simulations.



Hierarchal Models for the analysis of a power buss

Now we will build the hierarchal model of the wire.

Step 1: Draw the base schematic for the RLGC model and define each value as function of R, L and C.



Attributes

File

Object: Symbol <element>RESISTOR

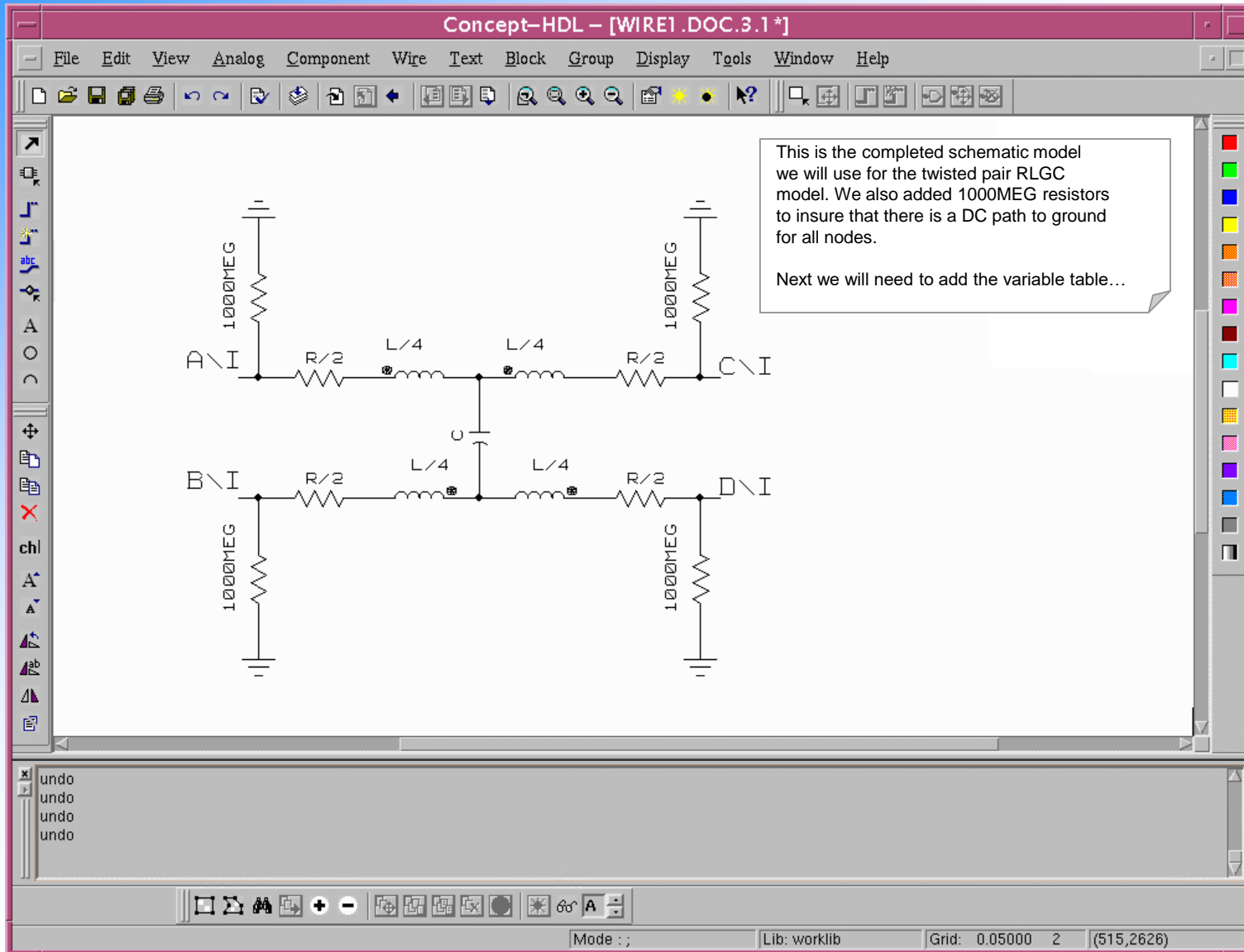
Name	Value	Visible	Align
VALUE	R/2	Value	Left
TC2	RTMPQ	None	Left
TC1	RTMPL	None	Left
MAX_TEMP	RTMAX	None	Left
SLOPE	RSMAX	None	Left
VOLTAGE	RVMAX	None	Left
POWER	RMAX	None	Left
DIST	FLAT	None	Left
NEGTOL	RTOL%	None	Left
POSTOL	RTOL%	None	Left
TOL_ON_OFF	ON	None	Left
PATH	R1	None	Left
SIZE	1B	None	Left
\$LOCATION	?	None	Left

OK Cancel Help

window out;
[attribute]
attr
attr



Hierarchical Models for the analysis of a power buss



Hierarchical Models for the analysis of a power buss

Concept-HDL - [WIRE1.DOC.3.1*]

File Edit View Analog Component Wire Text Block Group Display Tools Window Help

Passives...
Elements...
Profile...
Libraries...
Select...
Show/Hide...
Add Variable Table...
Add Properties...
Nodeset...
Initial Condition...

Attributes

File

Object: Symbol <element> VARIABLES

Name	Value	Visible	Align
C	$((\text{LENGTH} * 0.7065 * 10^{-12}) / (\text{LN}((2 * S) / \text{WD}))) * \text{ER}$	Both	Left
L	$(\text{LENGTH} * 10.16 * 10^{-9}) * \text{LN}((2 * S) / \text{WD})$	Both	Left
R	$(4 * \text{RO} * \text{LENGTH}) / (\text{PI} * \text{WD}^2)$	Both	Left
S	0.068	Both	Left
ER	2.55	Both	Left
WD	0.0501	Both	Left
RO	6.787E^{-7}	Both	Left
LENGTH	0	Both	Left
VTOL	0	None	Left
VMAX	12	None	Left
RVMAX	24	None	Left
RTMPQ	0	None	Left
RTMAX	200	None	Left
RSMAX	0.005	None	Left
RMAX	.25	None	Left

OK Cancel Help Add D

Step 2: Add the variable table and define the R, L and C values as functions of wire length.

Other variables are used to define R, L and C but only length will be passed through the body.

undo redo redo delete

Mode : delete Lib: worklib Grid: 0.05000 2 (670,3566)



Hierarchical Models for the analysis of a power buss

The screenshot shows the Concept-HDL software interface. The title bar reads "Concept-HDL - [WIRE1.DOC.3.1 *]". The menu bar includes File, Edit, View, Analog, Component, Wire, Text, Block, Group, Display, Tools, Window, and Help. The main workspace contains the following text:

```

DRAWING LAST_MODIFIED=Thu Oct  3 14:13:52 2002
WIRE1.SCH.1.1
⊕ User Variables:
LENGTH=0
RO=6.737E-7
WD=0.000001
SR=0.000001
SR=0.000001
R=<4*RO*LENGTH>/<PI*WD^2>
L=<LENGTH*10.16*10^-9>*LN<(2*S)/WD>
C=<<LENGTH*0.7065*10^-12>/<LN<(2*S)/WD>>)*ER

```

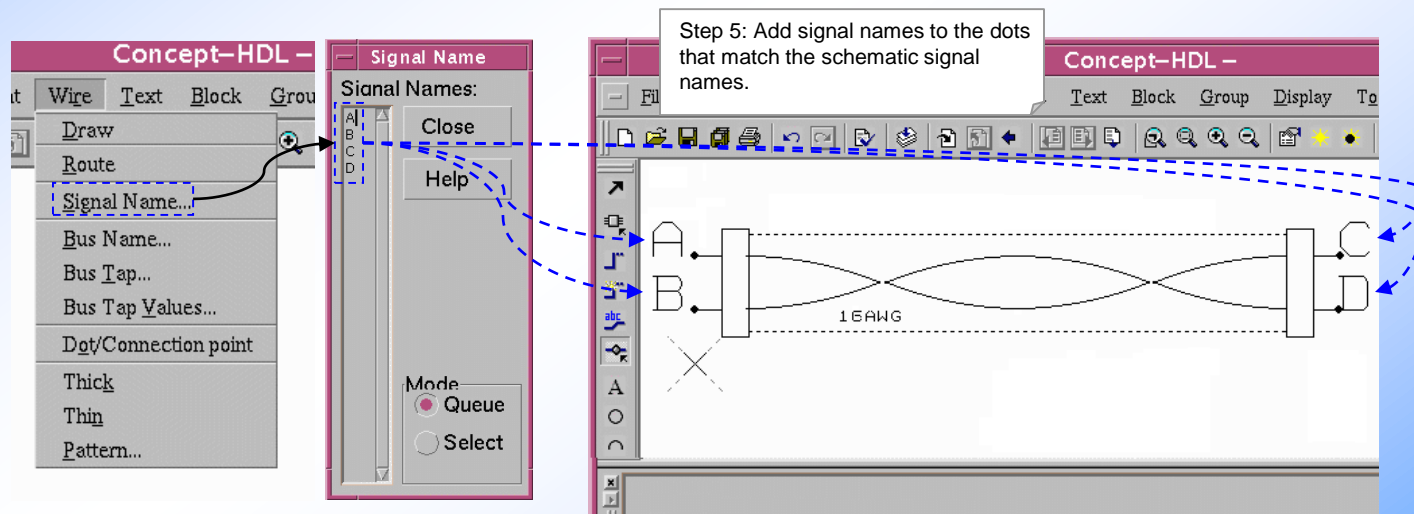
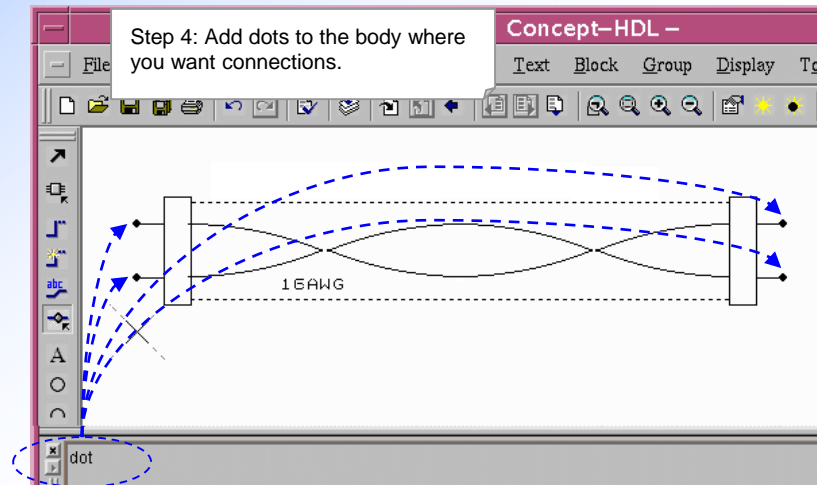
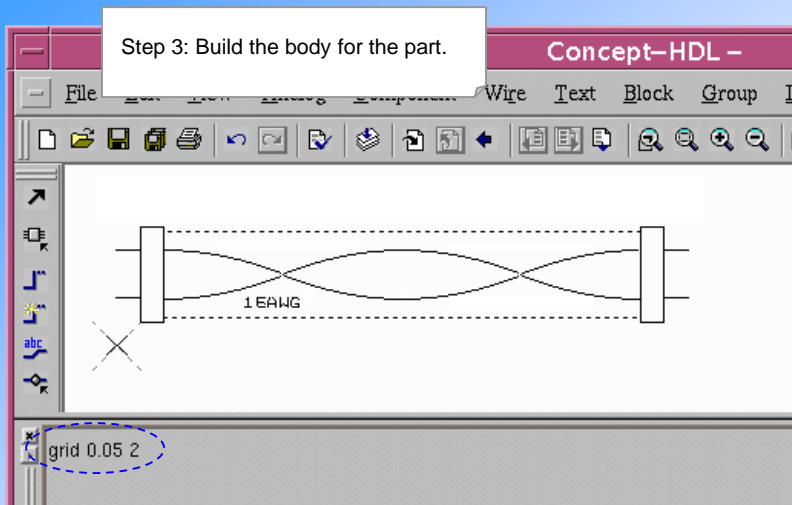
A callout box on the right contains the text: "Here is the completed schematic model with the variable table. Next we will need to build the body ...".

The schematic diagram shows a power bus with four terminals: A, B, C, and D. Each terminal is connected to a 1000MEG resistor to ground. The bus is modeled with resistors (R/2) and inductors (L/4) between the terminals. A central node is connected to ground through a capacitor (C).

The bottom status bar shows "Mode :", "Lib: worklib", "Grid: 0.05000 2", and "(37,2399)".



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Hierarchal Models for the analysis of a power buss

Concept-HDL -

File Edit View Analog Component Wire Text Block Group Display Tools Window

Attributes

Object: Symbol <standard>ORIGIN

Name	Value	Visible	Align
LENGTH	?\VARIABLE	Both	Left
PATH	?	None	Left
TOL_ON_OFF	ON	None	Left

OK Cancel Help Add

Step 6: Add path and length as properties to the body at the origin of the symbol.

Origin

LENGTH=?\VARIABLE

1.6AWG

chl

attr

Hierarchal Models for the analysis of a power buss

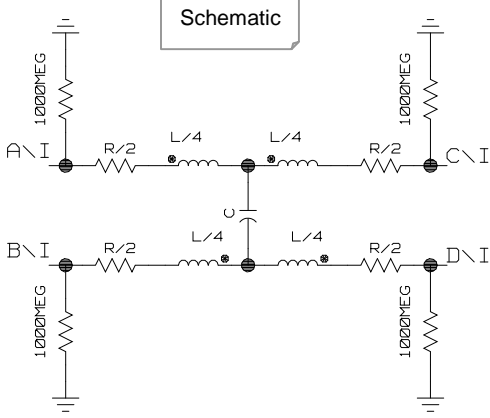
And your done.

```

_DRAWING_LAST_MODIFIED=Thu Oct 3 14:13:23 2002
WIRE1.SCH.1.1
User Variables:
LENGTH=10
RO=1.72E-7
WD=0.0501
S=0.0501
R=((4*RO*LENGTH)/(PI*WD^2))
L=((LENGTH*10.16*10^-9)*LN((2*S)/WD))
C=((LENGTH*0.7065*10^-12)/(LN((2*S)/WD)))*ER
    
```

This is an adaptation of the basic lumped element RLGC model which provides some minimum distributed impedances. G is not included.

Schematic



Only the values are shown.

1000Meg resistors added to model so all nodes would have a dc path to ground.

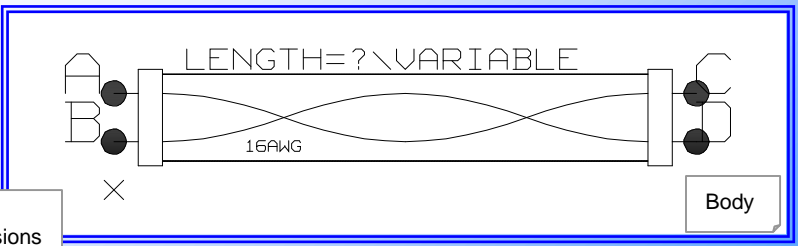
R, L and C are all functions of length so the equations for each can be written as expressions where length is a variable attached to the body of the model. Length can then be passed through the body to modify the R, L and C values.

Where,

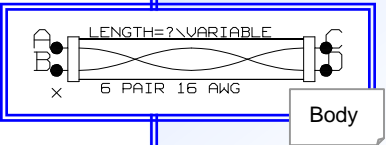
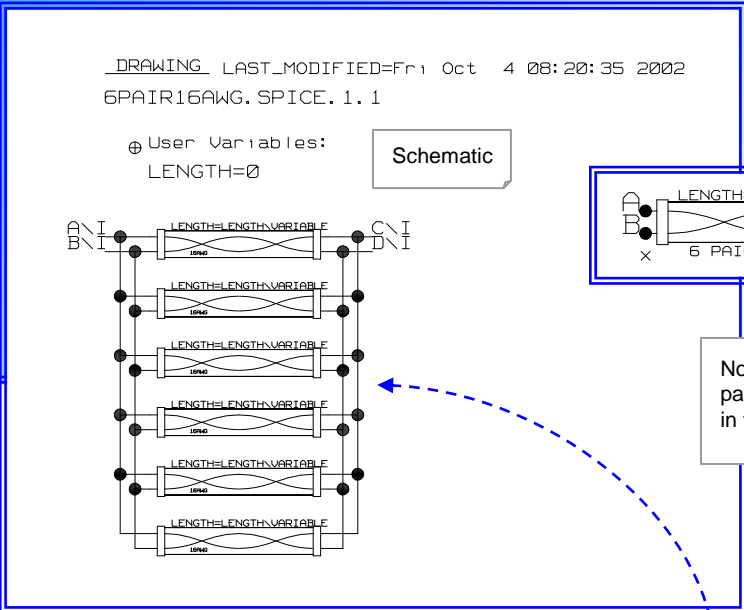
- RO = bulk resistivity of copper (ohm-in)
- WD = wire diameter (in)
- ER = effective relative dielectric constant of medium between wire in this case the insulation is ETFE (2.5 to 2.6)
- S = separation between the wires (in)

and

R, L and C are calculated based upon length...

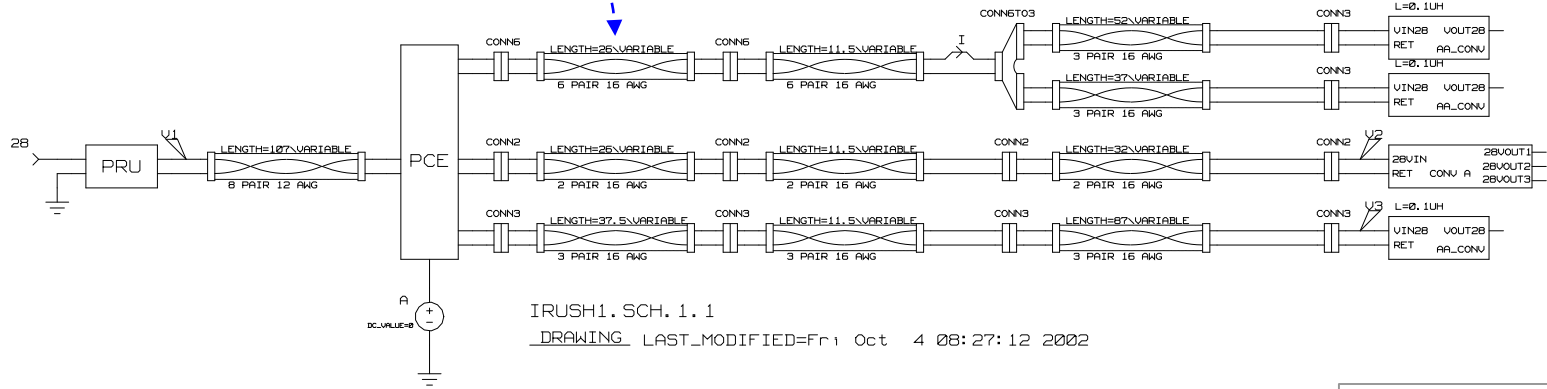


Hierarchal Models for the analysis of a power buss



Now we will expand the base twisted pair model to mimic the cables used in the system.

Once the base model is built it can be expanded in a hierarchal fashion to build more complicated models. In this case all the models used here are hierarchal.



hierarchal schematic

Imagine how complicated this schematic would be if it was drawn as a flat schematic



Hierarchal Models for the analysis of a power buss

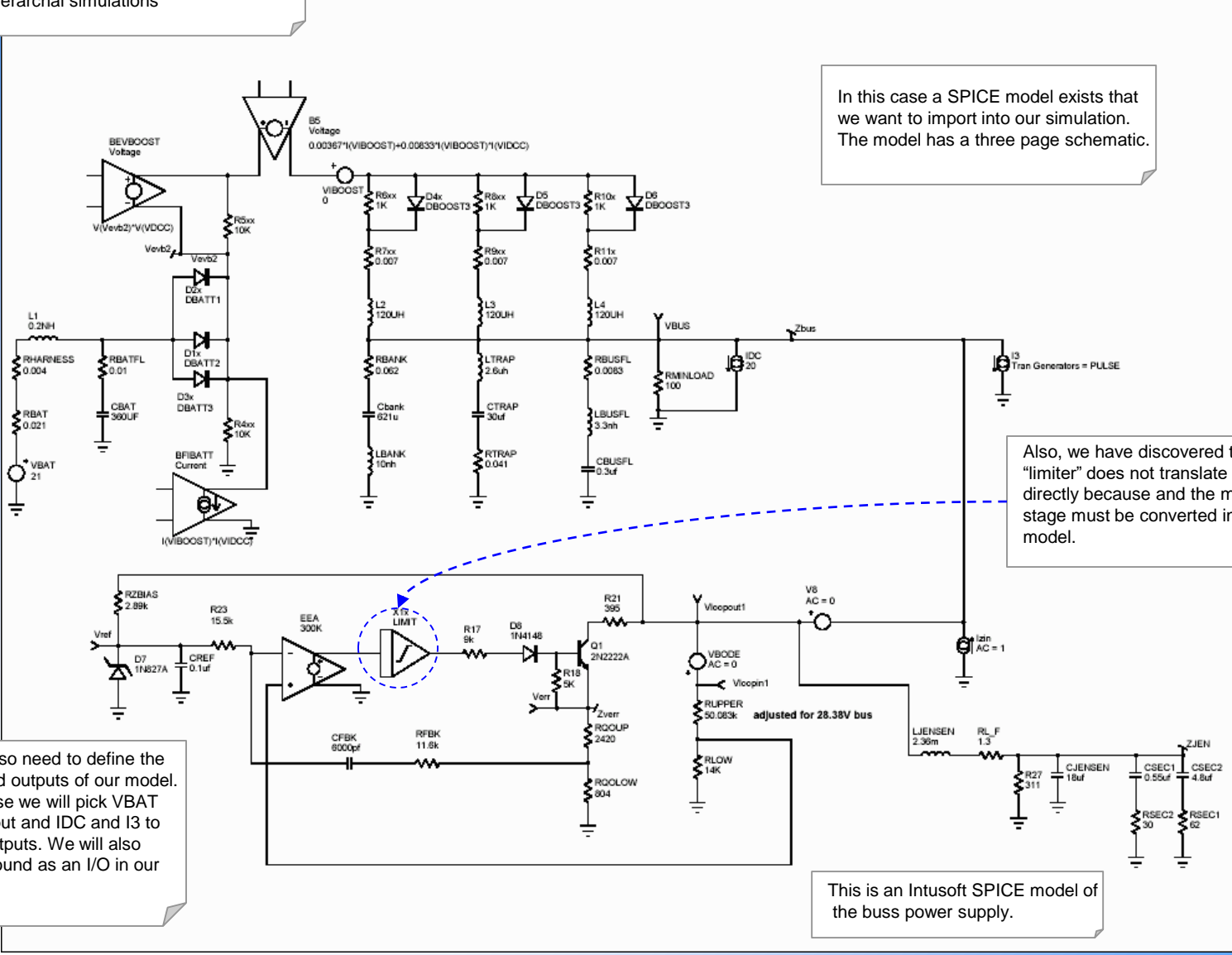
We were given a SPICE deck for one of the subsystems that we want to translate into AWB and place in our hierarchal simulations

In this case a SPICE model exists that we want to import into our simulation. The model has a three page schematic.

Also, we have discovered that the "limiter" does not translate into AWB directly because and the model for this stage must be converted into the AWB model.

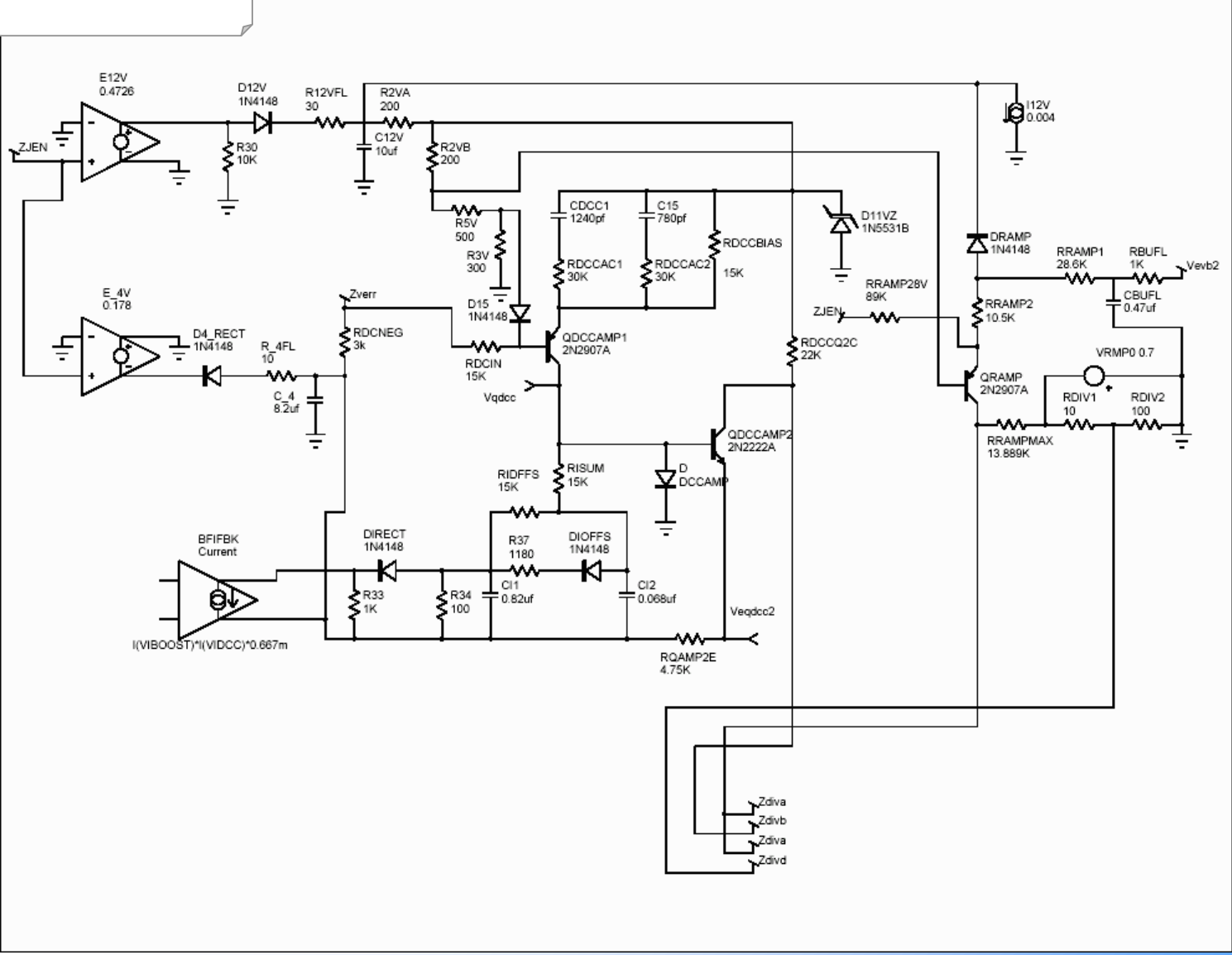
We will also need to define the inputs and outputs of our model. In this case we will pick VBAT as the input and IDC and I3 to be our outputs. We will also define ground as an I/O in our model.

This is an Intusoft SPICE model of the buss power supply.



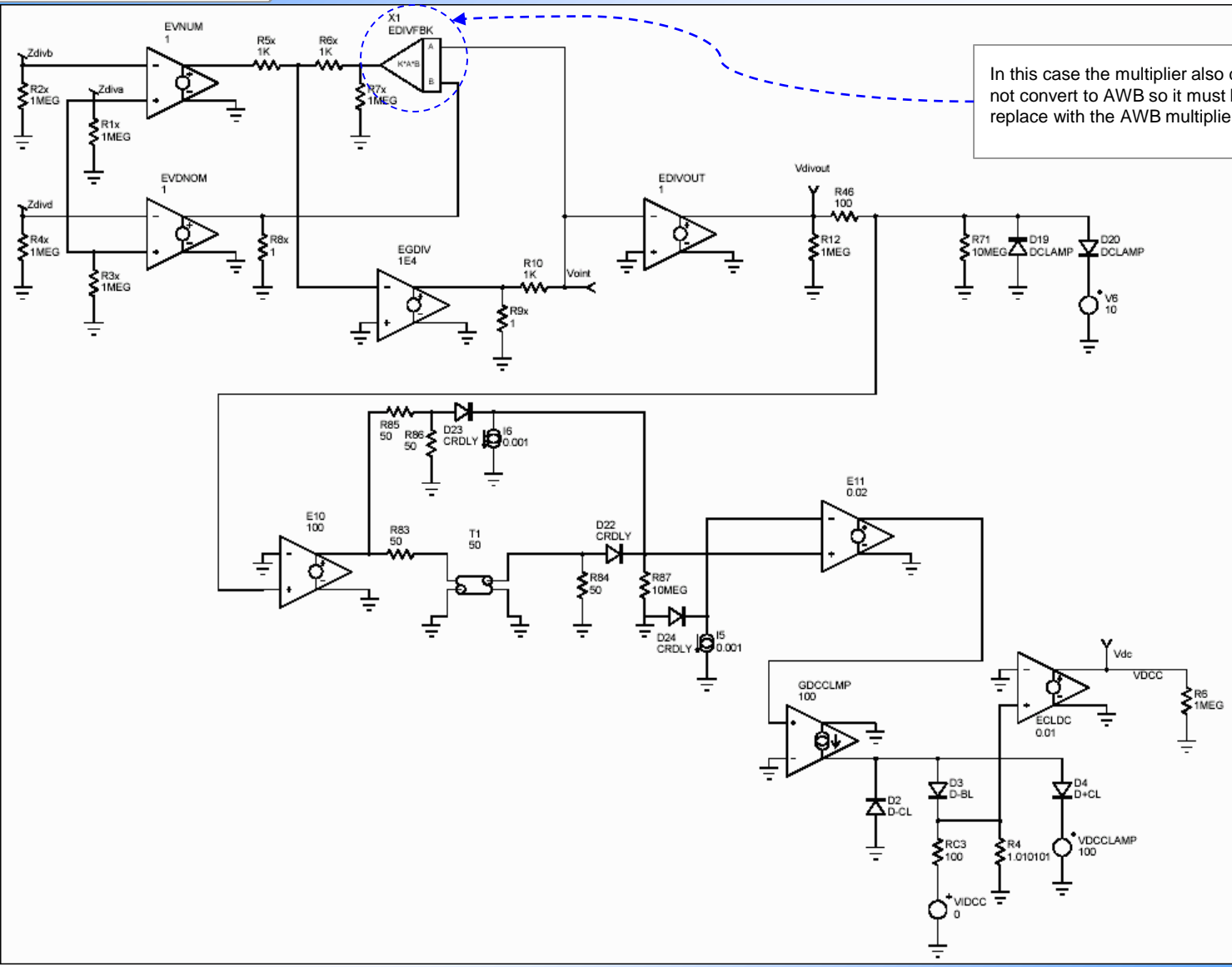
Hierarchal Models for the analysis of a power buss

Page two of the Intusoft model.



Hierarchal Models for the analysis of a power buss

Page three of the Intusoft model.



In this case the multiplier also does not convert to AWB so it must be replace with the AWB multiplier model.



Hierarchical Models for the analysis of a power buss

The SPICE deck for the model must be dissected to determine to translate it into the AWB format. With the exception of the two circuit models that don't translate directly we will also need to remove SPICE options and replace node names with node number which have not been used. A simple text editor can be used for this option.

```
*BOOST NOM, IDC=40A
*.NODESET V(VDCC)=0.3
*.NODESET V(44)=-2.0
*BOOST NOM, IDC=20A
.NODESET V(VDCC)=0.5
.NODESET V(50)=-2.6
.NODESET V(zverr)=7.0
.IC V(VDCC)=0.3 V(44)=-2.5
*#op
.OPTIONS itl1=1000
.OPTIONS gmin=10n reltol=0.01 rshunt=100meg
VBAT 1 0 DC=21
RBAT 1 2 0.021
RHARNES 2 3 0.004
L1 3 4 0.2NH
RBATFL 4 5 0.01
CBAT 5 0 360UF
D1x 4 Vevb2 _DBAT
.MODEL _DBAT D BV=45 CJO=5.915n IBV=1 IS=924.7n M=0.3333
+ RS=2.018m TT=417ps VJ=0.75
D2x 4 Vevb2 _DBAT
D3x 4 Vevb2 _DBAT
R4xx Vevb2 0 10K
R5xx Vevb2 7 10K
RBANK Zbus 15 0.062
BEVBOOST 7 Vevb2 V=V(Vevb2)*V(VDCC)
I3 Zbus 0 DC=0 PULSE 0 8 100US 1US 1US 400US
VIBOOST 8 9 DC=0
R6xx 9 10 1K
R7xx 10 11 0.007
L2 11 Zbus 120UH
D4x 9 10 _DMODBST
.MODEL _DMODBST D BV=150 CJO=1.457n IBV=100u IS=7.5u
+ M=0.3333 N=2 RS=0.1m TT=123.3n VJ=0.75
R8xx 9 13 1K
R9xx 13 14 0.007
L3 14 Zbus 120UH
D5 9 13 _DMODBST
R10x 9 16 1K
R11x 16 17 0.007
L4 17 Zbus 120UH
D6 9 16 _DMODBST
Cbank 15 18 621u
LBANK 18 0 10nh
```

```
LTRAP Zbus 20 2.6uh
CTRAP 20 21 30uf
RTRAP 21 0 0.041
RBUSFL Zbus 19 0.0083
LBUSFL 19 22 3.3nh
CBUSFL 22 0 0.3uf
RMINLOAD Zbus 0 100
IDC Zbus 0 DC=20
EEA 24 0 34 31 300K
RZBIAS 69 23 2.89k
D7 0 23 DN827A
.MODEL DN827A D BV=6.153 CJO=100P IBV=7.5M IS=4.07F M=.33
+ N=1 RS=6.54 TT=55.1N VJ=.75
CREF 23 0 0.1uf
X1x 24 25 LIMIT { K=1 PLIM=23 NLIM=0 }
.SUBCKT LIMIT 1 2 {K=??? PLIM=??? NLIM=???}
*Connections: In Out
*Parameters: K Gain, PLIM Positive rail in Volts, NLIM Negative rail in Volts
RIN 1 0 1E12
E1 3 0 0 1 {K}
RC1 2 4 1MEG
C1 2 4 1F IC=0
R1 3 4 1MEG
E2 2 0 0 4 1E6
*DIODES WILL HAVE .0597V DROP AT 10V INPUT FOR GAIN=1
*DIODE = IS*EXP(.597/.026)
VN 5 2 {NLIM-.0597}
DN 4 5 DN
.MODEL DN D(IS=1E-12 N=.14319)
VP 2 6 {PLIM-.0597}
DP 6 4 DN
.ENDS
R17 25 26 9k
D8 26 27 DN4148
.MODEL DN4148 D BV=100V CJO=4PF IS=7E-09 M=.45 N=2 RS=.8
+ TT=6E-09 VJ=.6V
Q1 30 27 Zverr QN2222A
.MODEL QN2222A NPN BF=205 BR=4 CJC=15.2P CJE=29.5P IKF=.5
+ IKR=.225 IS=81.1F ISE=10.6P NE=2 NF=1 NR=1 RB=1.37 RC=.137
+ RE=.343 TF=397P TR=85N VAF=113 VAR=24 XTB=1.5
R18 27 Zverr 5K
RQOUP Zverr 28 2420
RQOLOW 28 0 804
R21 30 69 395
```



You will also need to pay attention to the length of the lines in the SPICE deck. The "+" sign is used to concatenate lines.

```
RFBK 28 32 11.6k
CFBK 32 31 6000pf
R23 31 23 15.5k
VBODE 33 69 AC=0
RUPPER 33 34 50.083k
RLOW 34 0 14K
LJENSEN 69 35 2.36m
RL_F 35 ZJEN 1.3
R27 ZJEN 0 311
CJENSEN ZJEN 0 18uf
CSEC1 ZJEN 37 0 0.55uf
RSEC2 37 0 30
CSEC2 ZJEN 38 4.8uf
RSEC1 38 0 62
E12V 39 0 ZJEN 0 0.4726
E_4V 0 42 ZJEN 0 0.178
R30 39 0 10K
D12V 39 40 DN4148
R12VFL 40 41 30
C12V 41 0 10uf
D4_RECT 43 42 DN4148
R_4FL 43 44 10
C_4 44 0 8.2uf
BFIFBK 45 44 I=I(VIBOOST)*I(VIDCC)*0.667m
R33 45 44 1K
DIRECT 46 45 DN4148
R34 46 44 100
C11 46 44 0.82uf
RIDFFS 46 47 15K
C12 47 44 0.068uf
RQAMP2E 44 50 4.75K
R37 46 48 1180
DIOFFS 47 48 DN4148
RISUM 47 49 15K
QDCCAMP2 Zdivb 49 50 QN2222A
D 49 0 _DCLAMP
.MODEL _DCLAMP D CJO=1E-18 EG=0.1 IBV=100n IS=1u
+ M=0.3333 RS=100u TT=50ps VJ=0.75 XTI=0
QDCCAMP1 49 51 52 QN2907A
.MODEL QN2907A PNP BF=154 BR=4 CJC=20.8P CJE=15.6P
+ IKR=.21 IS=381F ISE=15.3P NE=2 NF=1 NR=1 RB=2.21
+ RE=.552 TF=636P TR=63.7N VAF=139 VAR=20 XTB=1.5
+ IKF=.14 RC=.221
RDCNEG 44 Zverr 3k
RDCIN Zverr 51 15K
```

```
RDCCAC1 52 53 30K
CDCC1 53 55 1240pf
RDCCAC2 52 54 30K
C15 54 55 780pf
RDCCBIAS 55 52 15K
RDCCQ2C 55 Zdivb 22K
R2VA 41 55 200
D11VZ 0 55 _D14_mod
.MODEL _D14_mod D BV=10.94 CJO=44.2P
+ IBV=1M IS=2.07N M=.33
+ N=1 RS=64.1 TT=50.1N VJ=1
R46 Zdivo 67 100
QRAMP Zdiva 57 60 QN2907A
D15 58 51 DN4148
R2VB 55 57 200
R5V 57 58 500
R3V 58 0 300
RRAMP2 60 61 10.5K
RRAMP28V ZJEN 60 89K
DRAMP 61 41 DN4148
I12V 41 0 DC=0.004
RRAMPMAX Zdiva 63 13.889K
RDIV1 63 Zdivd 10
RDIV2 Zdivd 0 100
RRAMP1 61 65 28.6K
RBUFL 65 Vevb2 1K
VRMP0 0 63 DC=0.7
CBUFL 65 0 0.47uf
BFIBATT Vevb2 0 I=I(VIBOOST)*I(VIDCC)
R71 67 0 10MEG
GDCCCLMP 0 72 73 0 100
D2 0 72 _DCLAMP
D3 72 86 _DCLAMP
B5 7 8 V=0.00367*I(VIBOOST)+0.00833*I(VIBOOST)*I(VIDCC)
V8 69 Zbus AC=0
EVNUM 71 0 Zdiva Zdivb 1
R1x Zdiva 0 1MEG
R2x Zdivb 0 1MEG
EVDNOM 74 0 Zdiva Zdivd 1
```

```
R3x Zdiva 0 1MEG
R4x Zdivd 0 1MEG
R5x 71 77 1K
R6x 77 78 1K
R7x 78 0 1MEG
EGDIV 79 0 0 77 1E4
X1 80 74 78 MUL { K=1 }
.SUBCKT MUL 1 2 3 {K=???}
*Connections: In1 In2 Out
*Parameters: K Gain
B1 3 0 V=V(1) * V(2) * {K}
.ENDS
R8x 74 0 1
R9x 79 0 1
R10 79 80 1K
EDIVOUT Zdivo 0 0 80 1
D19 0 67 _DCLAMP
R12 Zdivo 0 1MEG
RC3 86 87 100
D20 67 68 _DCLAMP
V6 68 0 DC=10
VIDCC 87 0 DC=0
R4 86 0 1.010101
D4 72 88 _DCLAMP
VDCCLAMP 88 0 DC=100
ECLDC VDCC 0 86 0 0.01
Izin 0 Zbus AC=1
R6 VDCC 0 1MEG
E10 59 0 67 0 100
R83 59 75 50
T1 75 0 76 0 ZO=50 TD=1U
R84 76 0 50
D22 76 81 _DCLAMP
R85 59 82 50
R86 82 0 50
D23 82 81 _DCLAMP
E11 73 0 81 85 0.02
R87 81 0 10MEG
D24 0 85 _DCLAMP
I5 85 0 DC=0.001
I6 81 0 DC=0.001
.END
```

Hierarchal Models for the analysis of a power buss



Hierarchal Models for the analysis of a power buss

Concept-HDL – [NEWPRU2.SYM.1.1 [in hierarchy]

File Edit View Analog Component Wire Text Block Group

Attributes

File

Object: Symbol <standard>ORIGIN

Name	Value	Visible	Align
PATH	?	None	Left

OK Cancel Help

VA VIN NEW PRU ZBUS ZBUS GND GND

attr

Select object Mode : attribute

```
start DEVICE_INFO
  MODEL_TYPE=570
  SYMBOL_NAME=newpru
end DEVICE_INFO
```

```
start TEXT PRE-ANALYSIS
```

```
RAW_SPICE :="
*VBAT 1 0 DC=21
RBAT 1 2 0.021
RHARNES 2 3 0.004
L1 3 4 0.2NH
RBATFL 4 5 0.01
CBAT 5 999 360UF
D1x 4 100 _DBAT
.MODEL _DBAT D BV=45 CJO=5.915n IBV=1 IS=924.7n M=0.3333
+ RS=2.018m TT=417ps VJ=0.75
.
.
.
15 85 999 DC=0.001
16 81 999 DC=0.001
* VA=1
* VEVB2=100
* ZVERR=200
* ZJEN=300
* ZBUS=400
* VDCC=500
* VIDCC=600
* Zdiva=700
* Zdivb=710
* Zdivd=720
* Zdivo=730
* GND=999
"
```

You can add comments to your SPICE deck by using the "*" at the start of a line...

Build the body to match the SPICE deck. Notice that the names on the body match the terminal names used on the body.

```
end TEXT PRE-ANALYSIS
```

```
start NODES
```

```
TERM(VA)=1
TERM(ZBUS)=400
TERM(GND)=999
end NODES
```

Hierarchal Models for the analysis of a power buss

Step 1: Add the following to the start of the SPICE deck...

```
start DEVICE_INFO
  MODEL_TYPE=570
  SYMBOL_NAME=newpru {you define this}
end DEVICE_INFO

start TEXT PRE-ANALYSIS

RAW_SPICE :="
(insert the SPICE deck here)
```

Step 2: Add the following to the end of the SPICE deck...

```
"
end TEXT PRE-ANALYSIS

start NODES
  TERM(VA)=1
  TERM(ZBUS)=400
  TERM(GND)=999
end NODES
```

Term are based on the I/O you have chosen.

Step 3: Move SPICE deck to UNIX side ...

Will need to do the DOS2UNIX command to eliminate line feeds

Step 4: Build model body ...

Test you new model and your done!



Hierarchal Models for the analysis of a power buss

Now we can simulate a very large design without having a complicated flat schematic to manage. Plus we have the option to change the wire length on any cable to determine how the performance of the system will change.

